

# Investigation of TeO<sub>2</sub>-Based Borotellurite Glass as a Radiation Shield: Effects of Composition on Attenuation Parameters

Oki Ade Putra<sup>1</sup>, Suci Faniandari<sup>1</sup>, Erik Bhekti Yutomo<sup>1</sup>

<sup>1</sup>Department of Physics, Faculty of Science and Mathematics, Diponegoro Univeristy, Semarang, Indonesia

Corresponding Author: Oki Ade Putra

DOI: <https://doi.org/10.52403/ijrr.20250351>

## ABSTRACT

The development of lead-free glass materials as radiation shielding has gained significant attention due to environmental concerns and the need for transparent shielding alternatives. This study investigates the effectiveness of TeO<sub>2</sub>-based borotellurite glass as a potential radiation shielding material. Glass samples with compositions of TeO<sub>2</sub>-(60-x) B<sub>2</sub>O<sub>3</sub>-20Bi<sub>2</sub>O<sub>3</sub>-15ZnO-5CaO (x = 0, 5, 10, 15 mol%) were synthesized and analyzed. The radiation shielding performance was evaluated using parameters attenuation within the energy range of 0.01–1.5 MeV. The obtained values were compared with those of commercial shielding materials, including RS-253-G18 glass and 40% synthetic borax. The results indicate that increasing TeO<sub>2</sub> concentration enhances the glass density and improves radiation attenuation capability. The TeB4 sample (15 mol% TeO<sub>2</sub>) exhibited the highest MAC value of 3.372 cm<sup>2</sup>/g at 0.06 MeV, which is significantly higher than that of TeB1 (2.814 cm<sup>2</sup>/g), TeB2 (3.011 cm<sup>2</sup>/g), and TeB3 (3.197 cm<sup>2</sup>/g). Additionally, the HVL values at 0.6 MeV for TeB1, TeB2, TeB3, and TeB4 were 1.390 cm, 1.359 cm, 1.329 cm, and 1.300 cm, respectively, confirming that higher TeO<sub>2</sub> concentration leads to a reduction in HVL and an overall improvement in shielding efficiency.

Moreover, the absorption edge of Bi<sub>2</sub>O<sub>3</sub> at 0.0905 MeV contributed to a sudden increase in attenuation efficiency at specific energy levels. The findings confirm that TeO<sub>2</sub>-based borotellurite glass is a promising candidate for radiation shielding applications, offering both high attenuation performance and optical transparency

**Keywords:** TeO<sub>2</sub>-based glass, radiation shielding, mass attenuation coefficient, borotellurite glass, and lead-free shielding materials

## INTRODUCTION

The utilization of ionizing radiation in various fields, including the medical industry (1) and food preservation (2), continues to increase. Along with this development, efforts to enhance protection for radiation workers have become highly important. Although ionizing radiation, such as gamma rays, offers various benefits, its uncontrolled use can negatively impact workers' health. There are three primary strategies for controlling ionizing radiation exposure: reducing exposure time, increasing the distance between workers and radiation sources, and using radiation shielding materials with optimal performance (3).

The combination of concrete and lead has long been used as a radiation shielding material due to its effectiveness in providing

protection for radiation workers. However, this material has several limitations, such as significant thickness, making it unsuitable for applications requiring limited space, its non-transparent nature, which hinders observation into radiation areas, and the toxic properties of lead, which pose potential health hazards to workers and the environment (4). Thus, glass-based radiation shielding emerges as a promising alternative as it is thinner, transparent, and allows for the use of lead-free fillers that are more environmentally friendly.

Numerous studies have been conducted to evaluate the effectiveness of glass as a radiation shielding material. Almuqrin et al. (2024) conducted a study on glass-based radiation shielding with a composition of B<sub>2</sub>O<sub>3</sub>-PbO-ZnO-CaO, where variations in ZnO concentration significantly increased the linear attenuation coefficient (LAC), with the highest value reaching 11.136 cm<sup>-1</sup> at a radiation energy of 0.060 MeV (5). Meanwhile, research by Sayyed (2025) developed glass shielding with a composition of 15BaO-10Na<sub>2</sub>O-5Al<sub>2</sub>O<sub>3</sub>-(70-x)B<sub>2</sub>O<sub>3</sub>-xCaO (where x = 5, 10, 15, and 20 mol%). The results indicated that increasing CaO concentration contributed to a reduction in the Half-Value Layer (HVL), leading to thinner glass shielding with more optimal radiation protection performance (6).

Tellurium dioxide (TeO<sub>2</sub>) is one of the materials used in glass systems for radiation shielding, primarily due to its superior physical and nuclear characteristics. With an atomic number of 52 and an atomic mass of 127.6, TeO<sub>2</sub> effectively absorbs high-energy radiation, such as gamma rays. Additionally, its high density makes it more efficient in shielding against radiation exposure compared to materials with lower atomic numbers. Other advantages include excellent thermal stability and chemical resistance, preventing degradation even in environments with high radiation exposure. Besides its radiation shielding properties, TeO<sub>2</sub> maintains transparency within the glass structure and possesses high

mechanical strength, making it ideal for radiation protection applications without compromising visibility or resistance to physical impacts (7).

This study aims to evaluate the effect of TeO<sub>2</sub> concentration variations on the performance of glass-based radiation shielding. The type of glass used in this study is borotellurite glass with a composition of TeO<sub>2</sub>-(60-x)B<sub>2</sub>O<sub>3</sub>-20Bi<sub>2</sub>O<sub>3</sub>-15ZnO-5CaO, where x = 0, 5, 10, and 15 mol%. Each oxide in this composition has a specific role in determining the physical, optical, and radiation shielding properties of the glass. TeO<sub>2</sub> serves as the primary glass former, increasing the density and optical transparency of the glass while also enhancing thermal stability and resistance to radiation exposure (7). B<sub>2</sub>O<sub>3</sub> acts as a network former, contributing to the glass structure, reducing melting temperature, and improving chemical stability and transparency. Bi<sub>2</sub>O<sub>3</sub> is added to enhance radiation shielding capability due to its high atomic number, making it effective in absorbing gamma radiation (8). According to Singh et al. (2023) and Alomayrah et al. (2024), ZnO changes the chemical stability of the glass and makes it more durable, while CaO changes the chemical stability of the glass and makes it stronger, more resistant to humidity, and helps make a more stable glass network (9) (10).

To assess the effectiveness of borotellurite glass as a radiation shield, various radiation absorption parameters were comprehensively calculated. The mass attenuation coefficient (MAC), the linear attenuation coefficient (LAC), the half-value layer (HVL), the tenth-value layer (TVL), and the mean free path (MFP) are all calculated in the energy range of 0.01 to 1.5 MeV. Simulations were conducted using XCOM software, which allows for the prediction of shielding characteristics based on physical parameters and material composition. The obtained results were then compared with various commercial shielding materials, including conventional glass shielding and concrete shielding, to

evaluate the effectiveness of borotellurite glass in radiation protection applications. This research is expected to serve as a primary reference in the development of glass shielding materials for future experimental applications.

## MATERIALS & METHODS

### Materials

The effect of TeO<sub>2</sub> concentration variations on the performance of glass-based radiation shielding was numerically evaluated using the XCOM software from the National Institute of Standards and Technology (NIST). This software provides mass attenuation coefficient (MAC) data, which

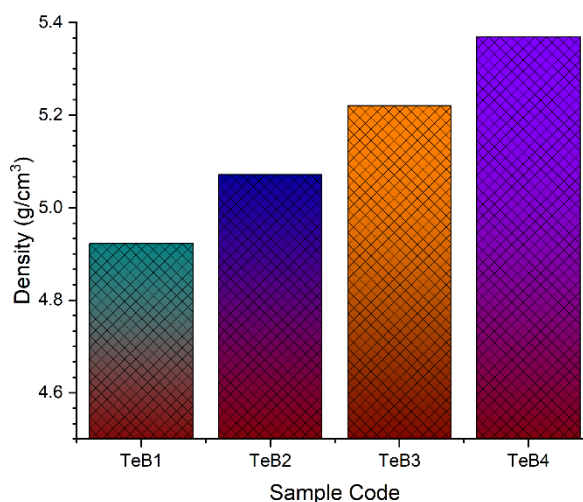
is then developed through analytical calculations to obtain other radiation absorption parameters, such as linear attenuation coefficient (LAC), half-value layer (HVL), tenth-value layer (TVL), and mean free path (MFP). This study involved four glass samples with varying TeO<sub>2</sub> concentrations, where each sample was analyzed within an energy range of 0.01–1.5 MeV. The chemical composition of each sample follows the general molecular formula TeO<sub>2</sub>-(60-x)B<sub>2</sub>O<sub>3</sub>-20Bi<sub>2</sub>O<sub>3</sub>-15ZnO-5CaO, with x = 0, 5, 10, and 15 mol%, while the mol% fraction and density of each sample are detailed in Table 1 and Figure 1.

**Table 1. Fraction of the Component (mol.%) and density of each sample**

Sample	TeO <sub>2</sub>	B <sub>2</sub> O <sub>3</sub>	Bi <sub>2</sub> O <sub>3</sub>	ZnO	CaO	Density (g/cm <sup>3</sup> )
TeB1	0	60	20	15	5	4.923
TeB2	5	55	20	15	5	5.071
TeB3	10	50	20	15	5	5.221
TeB4	15	45	20	15	5	5.370

Analysis based on Table 1 shows a correlation between the increase in TeO<sub>2</sub> concentration and the increase in the density of the shielding material, although there is a simultaneous decrease in B<sub>2</sub>O<sub>3</sub> fraction. TeB4, which has the highest TeO<sub>2</sub> concentration of 15 mol%, exhibits the highest density of 5.370 g/cm<sup>3</sup>, whereas the

densities of the other samples, TeB1, TeB2, and TeB3, are 4.923 g/cm<sup>3</sup>, 5.071 g/cm<sup>3</sup>, and 5.221 g/cm<sup>3</sup>, respectively. Information regarding the molar fraction of each element in the glass composition for each sample is presented in Table 2, which is then used as input in the XCOM software.



**Figure 1. Density of each sample**

## Methods

The XCOM software, developed by NIST, is a data-based program used to calculate scattering, photoelectric absorption, and pair production, as well as to determine the mass attenuation coefficient in the energy range

of 0.001 MeV to 20 MeV theoretically (11). This program serves as the basis for calculating radiation shielding parameters, which are then compared among samples to evaluate the effectiveness of shielding against ionizing radiation.

**Table 2. Fraction of the element (wt.%) of each element**

Sample	Te	O	B	Bi	Zn	Ca
TeB1	0	0.2774	0.0865	0.5574	0.0654	0.0133
TeB2	0.0413	0.2641	0.0769	0.5412	0.0635	0.0129
TeB3	0.0803	0.2516	0.0680	0.5258	0.0617	0.0126
TeB4	0.1171	0.2398	0.0595	0.5112	0.0601	0.0123

The radiation absorption parameters analyzed in this study include LAC, MAC, HVL, TVL, and MFP. LAC is a measure of how quickly ionizing radiation intensity decreases as it passes through a material, directly related to the material's ability to absorb or block radiation. The higher the LAC value, the more effective the material functions as radiation shielding. The LAC value can be obtained by applying Lambert-Beer's equation (12) as follows:

$$I = I_0 e^{-\mu x} \quad (1)$$

where  $I_0$  and  $I$  represent the initial and attenuated radiation intensities,  $\mu$  is the LAC ( $\text{cm}^{-1}$ ), and  $x$  is the thickness of the shielding material (cm).

The MAC parameter indicates how much a material can absorb radiation per unit density (13). Unlike LAC, which measures absorption based on the radiation path length in the material, MAC considers material density, providing a more general perspective in comparing the effectiveness of various shielding materials. The larger the MAC value, the better the material's quality in absorbing radiation. The MAC value is calculated by dividing LAC by the density of the material and considering the contribution of each component in the material based on its mass fraction. The MAC calculation formula is given as (10):

$$MAC = \frac{\mu}{\rho} = \sum_i w_i \left( \frac{\mu}{\rho} \right)_i \quad (2)$$

Additionally, other important parameters in evaluating shielding material performance are HVL and TVL, which indicate the thickness of the material required to reduce radiation intensity to half and one-tenth of its original value, respectively (14). The equations for calculating HVL and TVL are given as follows:

$$HVL = \frac{\ln 2}{\mu} \quad (3)$$

$$TVL = \frac{\ln 10}{\mu} \quad (4)$$

MFP represents the average distance traveled by radiation particles before interacting with atoms in the shielding material. The smaller the MFP value, the higher the material's ability to attenuate radiation exposure, as radiation interactions with the material occur over shorter distances. The MFP value can be determined using the following equation (15):

$$MFP = \frac{1}{\mu} \quad (5)$$

Evaluation of these parameters enables the determination of shielding material effectiveness in absorbing and reducing ionizing radiation intensity, as well as providing a basis for comparing various types of materials used in radiation protection applications.

## RESULT AND DISCUSSION

### Effect of TeO<sub>2</sub> Concentration Variations on Radiation Shielding Performance

The higher the mass attenuation coefficient (MAC) of a radiation shield, the more effective the material is in attenuating gamma rays (5). The MAC value is influenced by two primary factors: material density and radiation energy. The first factor, shielding material density, plays a crucial role in enhancing radiation shielding effectiveness. The higher the density of a

material, the greater the number of available electrons, thereby increasing the probability of interaction between photons and electrons in the material. Figure 2 shows that the TeB4 sample has the highest density, which directly contributes to the increased MAC value. At 0.06 MeV radiation energy, the MAC value for TeB4 is recorded at 3.372 cm<sup>2</sup>/g, which is higher than the MAC values of other samples, namely TeB1 (2.814 cm<sup>2</sup>/g), TeB2 (3.011 cm<sup>2</sup>/g), and TeB3 (3.197 cm<sup>2</sup>/g).

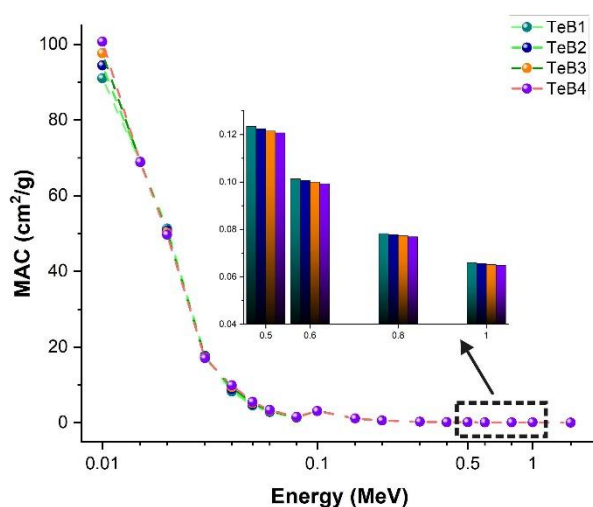


Figure 2. Mass attenuation coefficient (MAC) in the radiation energy range of 0.01 – 1.5 MeV

The second factor influencing MAC values is radiation energy. From Figure 2, it is evident that in the same sample, such as TeB2, the MAC value initially measures 94.430 cm<sup>2</sup>/g at 0.01 MeV, but then decreases to 0.051 cm<sup>2</sup>/g at 1.5 MeV. This reduction in MAC is attributed to the varying types of radiation-matter interactions, which differ based on energy levels. At low energy levels, the dominant interaction is the photoelectric effect (PE), where photons disappear after transferring their entire energy to electrons within the material. The effectiveness of the photoelectric effect in attenuating radiation follows an inverse relationship with radiation energy ( $\sigma_{PE} \propto 1/E$ ) (16). At moderate energy levels, the dominant interaction shifts to Compton scattering

(CS), which is influenced by the effective atomic number ( $Z_{eff}$ ) with the relationship ( $\sigma_{CS} \propto Z_{eff}$ ) (8). As radiation energy increases further, the dominant interaction becomes pair production, which occurs when photons possess energy exceeding 1.022 MeV, resulting in the formation of electron-positron pairs (17).

Additionally, Figure 2 also shows a sudden increase in MAC values at 0.1 MeV, which is caused by the absorption edge of bismuth (Bi) in Bi<sub>2</sub>O<sub>3</sub>, located at the K-shell energy level of 0.0905 MeV. The absorption edge plays a crucial role in determining how effectively a material absorbs X-rays and gamma rays, particularly at low-to-medium energy levels where photoelectric interactions are more dominant.



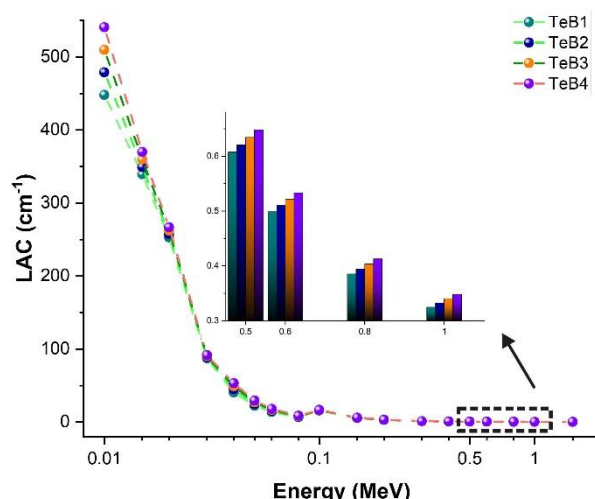


Figure 3. Linear attenuation coefficient (LAC) in the radiation energy range of 0.01 – 1.5 MeV

The MAC values obtained from numerical calculations using XCOM software were subsequently used to compute the linear attenuation coefficient (LAC) using Equation (2). The LAC values exhibit a trend similar to MAC, where an increase in radiation energy corresponds to a decrease in LAC (12). Figure 3 illustrates that for the TeB2 sample, the LAC initially measures 478.901 cm<sup>-1</sup> at 0.01 MeV, but declines to 0.258 cm<sup>-1</sup> at 1.5 MeV. Unlike MAC, the LAC values are not influenced by material density, but rather by the molar fraction of TeO<sub>2</sub> compounds in the composition of the glass radiation shield. At 0.5 MeV, the LAC values for each sample are recorded as follows: TeB1 (0.607 cm<sup>-1</sup>), TeB2 (0.621 cm<sup>-1</sup>), TeB3 (0.634 cm<sup>-1</sup>), and TeB4 (0.648 cm<sup>-1</sup>), indicating that increasing TeO<sub>2</sub> concentration contributes to an increase in LAC values.

Thus, the results of the analysis demonstrate that MAC and LAC values are influenced by a combination of material density, molar fraction of constituent components, and received radiation energy, with TeB4 exhibiting the best performance in absorbing low-to-medium energy radiation. This finding suggests that Bi<sub>2</sub>O<sub>3</sub>-TeO<sub>2</sub>-based glass could be a potential candidate for high-efficiency radiation shielding.

### Effect of Material Density and Radiation Energy on Half-Value Layer (HVL) and Tenth-Value Layer (TVL) in Glass-Based Radiation Shielding

The smaller the half-value layer (HVL) of a material, the more effective it functions as a radiation shield (14). HVL is influenced by two main factors: material density and photon radiation energy. The first factor is shielding material density, where the higher the density of a material, the greater the probability of interaction between gamma radiation and electrons within the material. This leads to a decrease in HVL values, as radiation weakens more rapidly when passing through denser materials (16). Based on Figure 4, at a radiation energy of 0.6 MeV, the HVL values for the samples TeB1, TeB2, TeB3, and TeB4 are 1.390 cm, 1.359 cm, 1.329 cm, and 1.300 cm, respectively. These results indicate that increased density due to the addition of TeO<sub>2</sub> contributes to the reduction in HVL values, demonstrating that Te plays an essential role in improving the effectiveness of radiation shielding. However, on the other hand, an increase in the molar fraction of TeO<sub>2</sub> also leads to a decrease in the molar fraction of B<sub>2</sub>O<sub>3</sub>, which may affect the physical and optical properties of the material.

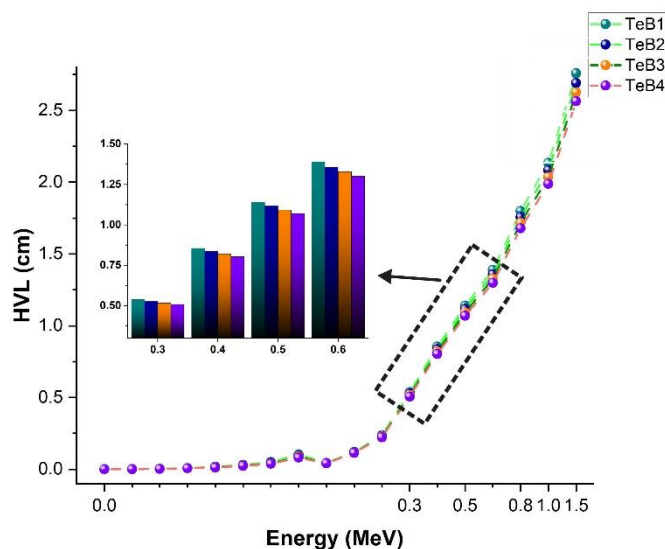


Figure 4. Half-value layer (HVL) in the radiation energy range of 0.01 – 1.5 MeV

The second factor affecting HVL values is radiation energy. The higher the radiation energy, the thicker the material required to reduce radiation intensity to half, resulting in an increase in HVL values. For instance, in the TeB4 sample, HVL increases with the

rise in received radiation energy. At 0.01 MeV, the HVL value is only 0.001 cm, but it increases to 2.564 cm at 1.5 MeV. This data indicates that thicker shielding materials are required to maintain effective protection against high-energy radiation.

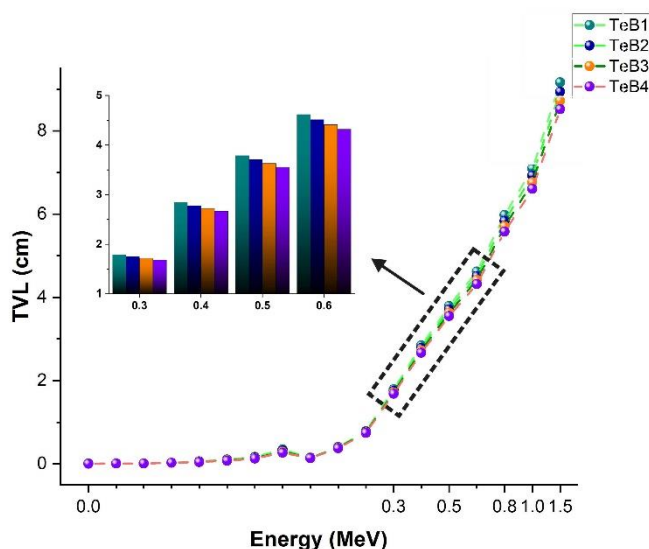


Figure 5. Tenth-value layer (TVL) in the radiation energy range of 0.01 – 1.5 MeV

Apart from HVL, another parameter with similar characteristics is the tenth-value layer (TVL). TVL represents the thickness of a material required to reduce radiation intensity to one-tenth of its initial value (18). In Figure 5, the TVL trend is similar to HVL, where TVL increases as radiation energy increases. However, at the same

energy level, TVL values decrease as the material density and TeO<sub>2</sub> concentration increase, indicating improved radiation shielding effectiveness due to the addition of Te elements in the glass material.

### Evaluation of Mean Free Path (MFP) in TeO<sub>2</sub>-Based Glass Radiation Shielding Compared to Commercial Shielding Materials

To evaluate the mean free path (MFP) of TeO<sub>2</sub>-based shielding, a comparison was made with commercial glass RS-253-G18 (19) and 40% synthetic borax (20). The analysis was conducted at two photon energy levels, 0.662 MeV and 1.332 MeV, to assess the effect of TeO<sub>2</sub> concentration on radiation shielding performance. At 0.662 MeV, an increase in TeO<sub>2</sub> concentration in the shielding material resulted in a decrease in MFP values, indicating improved radiation shielding effectiveness. According to Figure 6, the TeB1 sample, which does not contain TeO<sub>2</sub>, has the highest MFP value of 2.203 cm, while the MFP values for the TeO<sub>2</sub>-containing samples are TeB2

(2.153 cm), TeB3 (2.105 cm), and TeB4 (2.059 cm), respectively. Compared to other radiation shielding materials, such as RS-253-G18 glass (4.800 cm) and 40% synthetic borax (5.500 cm), all TeO<sub>2</sub>-based samples exhibit lower MFP values, indicating that TeO<sub>2</sub>-based shielding is more effective in attenuating radiation. The smaller the MFP value, the better the material quality as a radiation shield (15). Additionally, simulation results indicate that TeO<sub>2</sub>-based shielding glass exhibits superior quality compared to other commercial shields. An additional advantage of TeO<sub>2</sub>-based glass is its transparent and flexible characteristics, making it more favorable for various applications compared to conventional radiation shields, which tend to be more rigid.

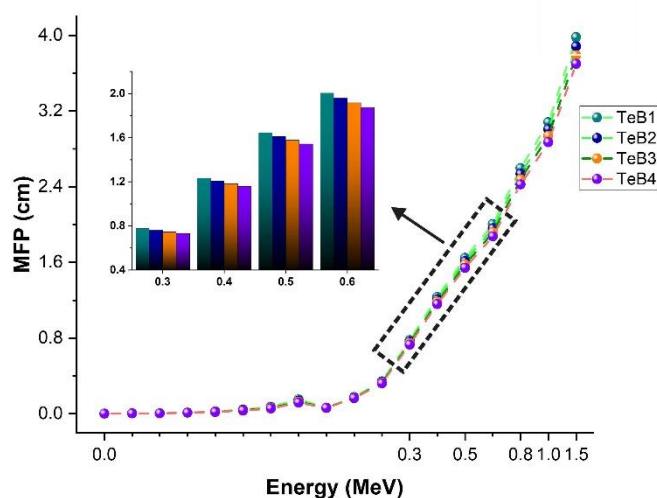


Figure 6. Mean free path (MFP) in the radiation energy range of 0.01 – 1.5 MeV

At 1.332 MeV, a similar trend is observed, where MFP decreases as the TeO<sub>2</sub> concentration increases in the shielding material. TeB4 has the lowest MFP value of 3.468 cm, which is smaller than other samples, specifically TeB1 (3.728 cm), TeB2 (3.637 cm), and TeB3 (3.550 cm). The MFP values of commercial RS-253-G18 glass (7.800 cm) and 40% synthetic borax (8.200 cm) remain significantly higher than TeO<sub>2</sub>-based shielding, confirming that TeO<sub>2</sub>-based glass is more

effective in absorbing radiation. This effectiveness is primarily attributed to the increase in material density due to TeO<sub>2</sub> addition, which enhances the probability of interaction between radiation photons and electrons within the material.

When analyzing a single sample, such as TeB3, the MFP value increases as the incident radiation energy rises. At 0.01 MeV, the MFP value is initially only 0.002 cm, but it increases to 3.789 cm at 1.5 MeV. This increase in MFP values indicates that



radiation particles travel longer distances before interacting with the shielding material, signifying a decline in radiation shielding effectiveness at higher energy levels. Therefore, these results confirm that TeO<sub>2</sub>-based glass demonstrates high efficiency in absorbing low-to-medium energy radiation, whereas for higher energy levels, materials with greater density may be required to maintain radiation protection effectiveness.

## CONCLUSION

The results demonstrated that increasing TeO<sub>2</sub> concentration enhances the density of the glass and significantly improves its ability to attenuate radiation. The TeB4 sample (15 mol% TeO<sub>2</sub>) exhibited the highest mass attenuation coefficient (MAC) of 3.372 cm<sup>2</sup>/g at 0.06 MeV, which was higher than the values obtained for the other samples. Additionally, the half-value layer (HVL) at 0.6 MeV showed a decreasing trend with increasing TeO<sub>2</sub> concentration, with values of 1.390 cm, 1.359 cm, 1.329 cm, and 1.300 cm for TeB1, TeB2, TeB3, and TeB4, respectively. These findings confirm that TeO<sub>2</sub> incorporation contributes to better radiation attenuation, making the glass an effective alternative for radiation shielding. The presence of Bi<sub>2</sub>O<sub>3</sub> in the glass composition resulted in an absorption edge at 0.0905 MeV, leading to a sudden increase in attenuation efficiency at lower energy levels. Moreover, a comparison with commercial shielding materials, including RS-253-G18 glass and 40% synthetic borax, showed that TeO<sub>2</sub>-based borotellurite glass exhibited lower mean free path (MFP) values, confirming its superior shielding capability. The material also offers the advantage of optical transparency, making it suitable for applications requiring both radiation protection and visibility. Based on these results, TeO<sub>2</sub>-based borotellurite glass emerges as a promising lead-free alternative to conventional shielding materials, offering high radiation attenuation, reduced HVL, and improved transparency. Future research should focus on experimental validation,

mechanical stability assessments, and optimization of glass compositions to further enhance its performance for practical applications in medical, nuclear, and industrial settings.

## Declaration by Authors

**Acknowledgement:** The authors sincerely thank the Physics Department, Faculty of Science and Mathematics, Diponegoro University for providing a supportive research environment and essential facilities

**Source of Funding:** None

**Conflict of Interest:** The authors declare no conflict of interest.

## REFERENCES

1. Nuñez-Briones AG, Benavides R, Bolaina-Lorenzo ED, Martínez-Pardo ME, Kotzian-Pereira-Benavides C, Mendoza-Mendoza E, et al. Nontoxic flexible PVC nanocomposites with Ta<sub>2</sub>O<sub>5</sub> and Bi<sub>2</sub>O<sub>3</sub> nanoparticles for shielding diagnostic X-rays. *Radiat Phys Chem.* 2023 Jan; 202:110512.
2. Al-Buriah MS, Kurtulus R, Eke C, Alomairy S, Olarinoye IO. An insight into advanced glass systems for radiation shielding applications: A review on different modifiers and heavy metal oxides-based glasses. *Heliyon.* 2024 Nov;10(22): e40249.
3. Dong M, Zhou S, Xue X, Feng X, Yang H, Sayyed MI, et al. Upcycling of boron bearing blast furnace slag as highly cost-effective shield for protection of neutron radiation hazard: An innovative way and proposal of shielding mechanism. *J Clean Prod.* 2022 Jun 25; 355:131817.
4. Wani AL, Ara A, Usmani JA. Lead toxicity: a review. *Interdiscip Toxicol.* 2015 Jun 1;8(2):55–64.
5. Almuqrin AH, Sayyed MI, Alharbi FF, Elsafi M. Experimental evaluation of the impact of ZnO on the radiation shielding ability of B<sub>2</sub>O<sub>3</sub>-PbO-ZnO-CaO glass systems. *Opt Mater.* 2024 Nov; 157:116213.
6. Sayyed MI, Maghrbi Y. Studying the impact of CaO on the radiation-shielding properties of BaO-Na<sub>2</sub>O-Al<sub>2</sub>O<sub>3</sub>-B<sub>2</sub>O<sub>3</sub>-CaO glasses using Eu-152 energy source. *Radiat Phys Chem.* 2025 Apr; 229:112475.

7. Ngaram SM, Hashim S, Sanusi MSM, Ibrahim A. Enhanced physical, optical and radiation shielding properties of tungsten modified potassium boro-tellurite glass systems: Theoretical approach. *Radiat Phys Chem.* 2025 Jan; 226:112355.
8. Yin S, Wang H, Wang S, Zhang J, Zhu Y. Effect of B<sub>2</sub>O<sub>3</sub> on the Radiation Shielding Performance of Telluride Lead Glass System. *Crystals.* 2022 Jan 26;12(2):178.
9. Singh RU, Sekhar KC, Alzahrani JS, Alrowaili ZA, Shareefuddin Md, Purushotham Y, et al. Effect of MoO<sub>3</sub> on Na<sub>2</sub>O–B<sub>2</sub>O<sub>3</sub>–CdO–ZnO glasses: Applications in optoelectronics, communication devices, and radiation shielding. *Ceram Int.* 2023 Apr;49(7):11600–11.
10. Alomayrah N, Albarqi MM, Alsulami RA, Alrowaili ZA, Eke C, Kebaili I, et al. Effect of CaF<sub>2</sub> on the radiation attenuation properties of SiO<sub>2</sub>–P<sub>2</sub>O<sub>5</sub>–CaO–Na<sub>2</sub>O bioactive glasses: Theoretical and simulation studies. *Results Phys.* 2024 Mar; 58:107441.
11. Şengül A. Gamma-ray attenuation properties of polymer biomaterials: Experiment, XCOM and GAMOS results. *J Radiat Res Appl Sci.* 2023 Dec;16(4):100702.
12. Kamaruddin KE, Kok SY, Ramli RM, Noor Azman NZ. X-ray attenuation measurement of electrospun polymer composite mats containing Bi<sub>2</sub>O<sub>3</sub>/WO<sub>3</sub> nanofillers as X-ray shielding material. *Appl Phys A.* 2024 Jun;130(6):455.
13. Alsaab AH, Zeghib S. Study of Prepared Lead-Free Polymer Nanocomposites for X- and Gamma-ray Shielding in Healthcare Applications. *Polymers.* 2023 Apr 29;15(9):2142.
14. Hou Y, Li M, Gu Y, Yang Z, Li R, Zhang Z. Gamma Ray Shielding Property of Tungsten Powder Modified Continuous Basalt Fiber Reinforced Epoxy Matrix Composites. *Polym Compos* [Internet]. 2018 Dec [cited 2024 Sep 26];39(S4). Available from: <https://4spublicationsonlineibrary.wiley.com/doi/10.1002/pc.24469>
15. Ahmed SN. Interaction of radiation with matter. In: *Physics and Engineering of Radiation Detection* [Internet]. Elsevier; 2015 [cited 2024 Oct 31]. p. 65–155. Available from: <https://linkinghub.elsevier.com/retrieve/pii/B9780128013632000024>
16. Alsaif NAM, Alotiby M, Hanfi MY, Mahmoud KA, Al-Yousef HA, Alotaibi BM, et al. Comprehensive study of radiation shielding and mechanical features of Bi<sub>2</sub>O<sub>3</sub>-TeO<sub>2</sub>-B<sub>2</sub>O<sub>3</sub>-GeO<sub>2</sub> glasses. *J Aust Ceram Soc.* 2021 Sep;57(4):1267–74.
17. Kaur P, Singh D, Singh T. Heavy metal oxide glasses as gamma rays shielding material. *Nucl Eng Des.* 2016 Oct; 307:364–76.
18. Fathy IN, El-Sayed AA, Elfakharany ME, Mahmoud AA, Abouelnour MA, Mahmoud AS, et al. Enhancing mechanical properties and radiation shielding of high-strength concrete with bulk lead oxide and granodiorite. *Nucl Eng Des.* 2024 Dec; 429:113626.
19. Hegazy HH, Al-Buriahi MS, Alresheedi F, El-Agawany FI, Sriwunkum C, Neffati R, et al. Nuclear shielding properties of B<sub>2</sub>O<sub>3</sub>–Bi<sub>2</sub>O<sub>3</sub>–SrO glasses modified with Nd<sub>2</sub>O<sub>3</sub>: Theoretical and simulation studies. *Ceram Int.* 2021 Jan;47(2):2772–80.
20. Singh KJ, Singh N, Kaundal RS, Singh K. Gamma-ray shielding and structural properties of PbO–SiO<sub>2</sub> glasses. *Nucl Instrum Methods Phys Res Sect B Beam Interact Mater At.* 2008 Mar;266(6):944–8.

How to cite this article: Oki Ade Putra, Suci Faniandari, Erik Bhukti Yutomo. Investigation of TeO<sub>2</sub>-Based borotellurite glass as a radiation shield: effects of composition on attenuation parameters. *International Journal of Research and Review.* 2025; 12(3): 414-423. DOI: <https://doi.org/10.52403/ijrr.20250351>

\*\*\*\*\*